



COM783 – Modelagem de Ligas com Memória de Forma

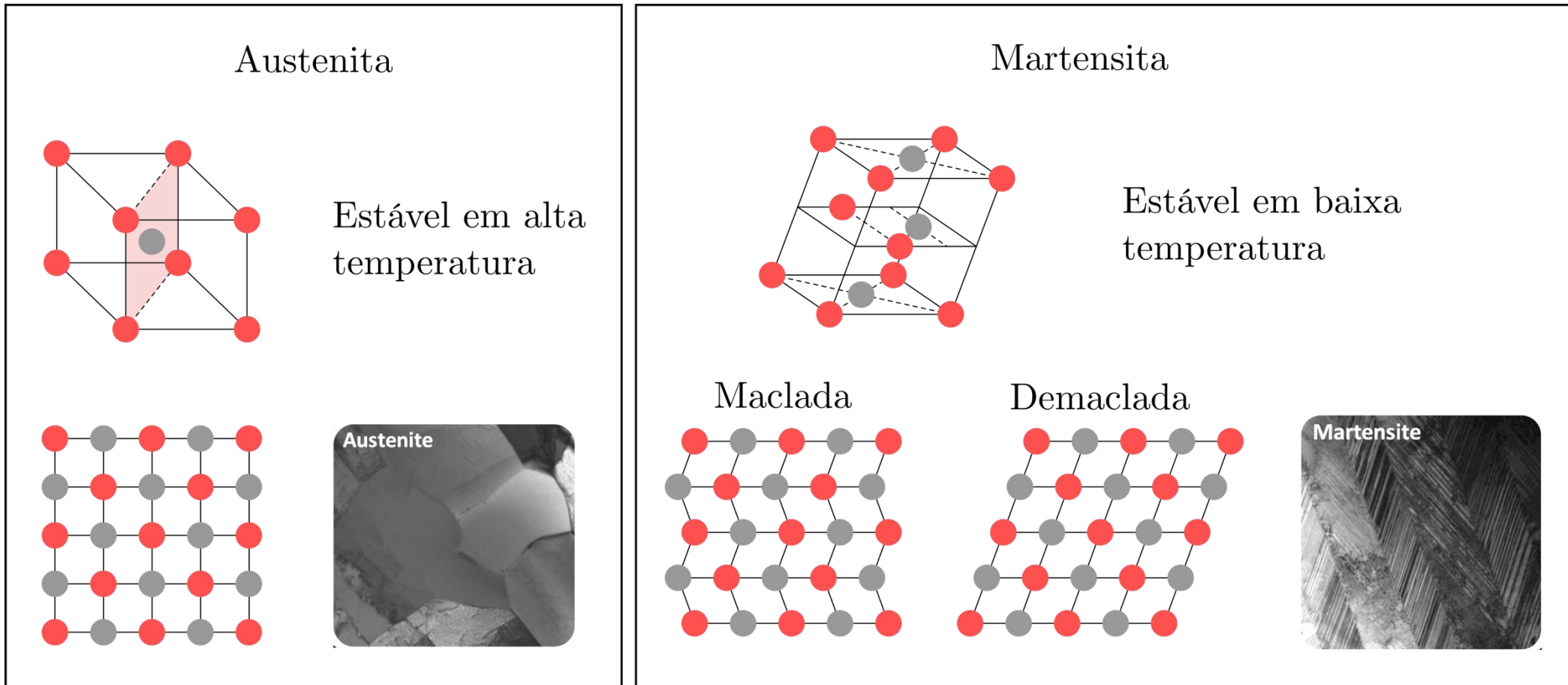
Prof. Luã G. Costa

Universidade Federal do Rio de Janeiro (COPPE/UFRJ)

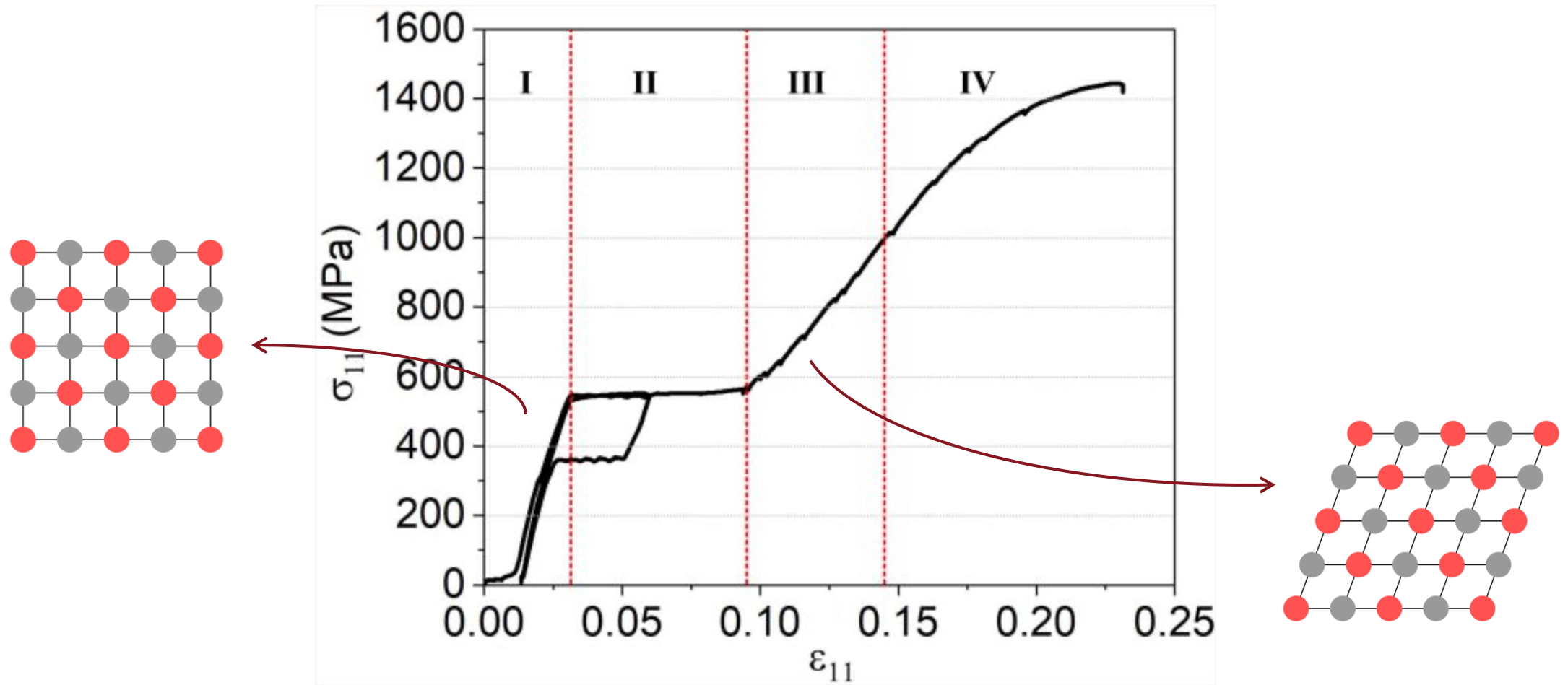
Programa de Engenharia Mecânica (PEM)

Deformação em Ligas com Memória de Forma

→ Mecanismo de transformação de fase tipo sólido-sólido



Deformação em Ligas com Memória de Forma

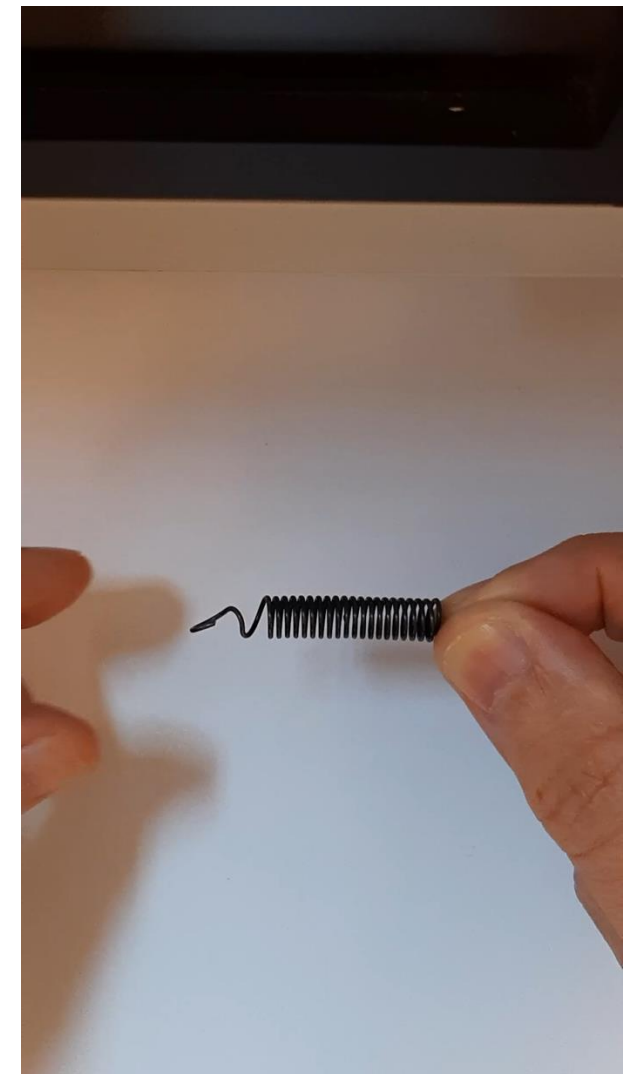
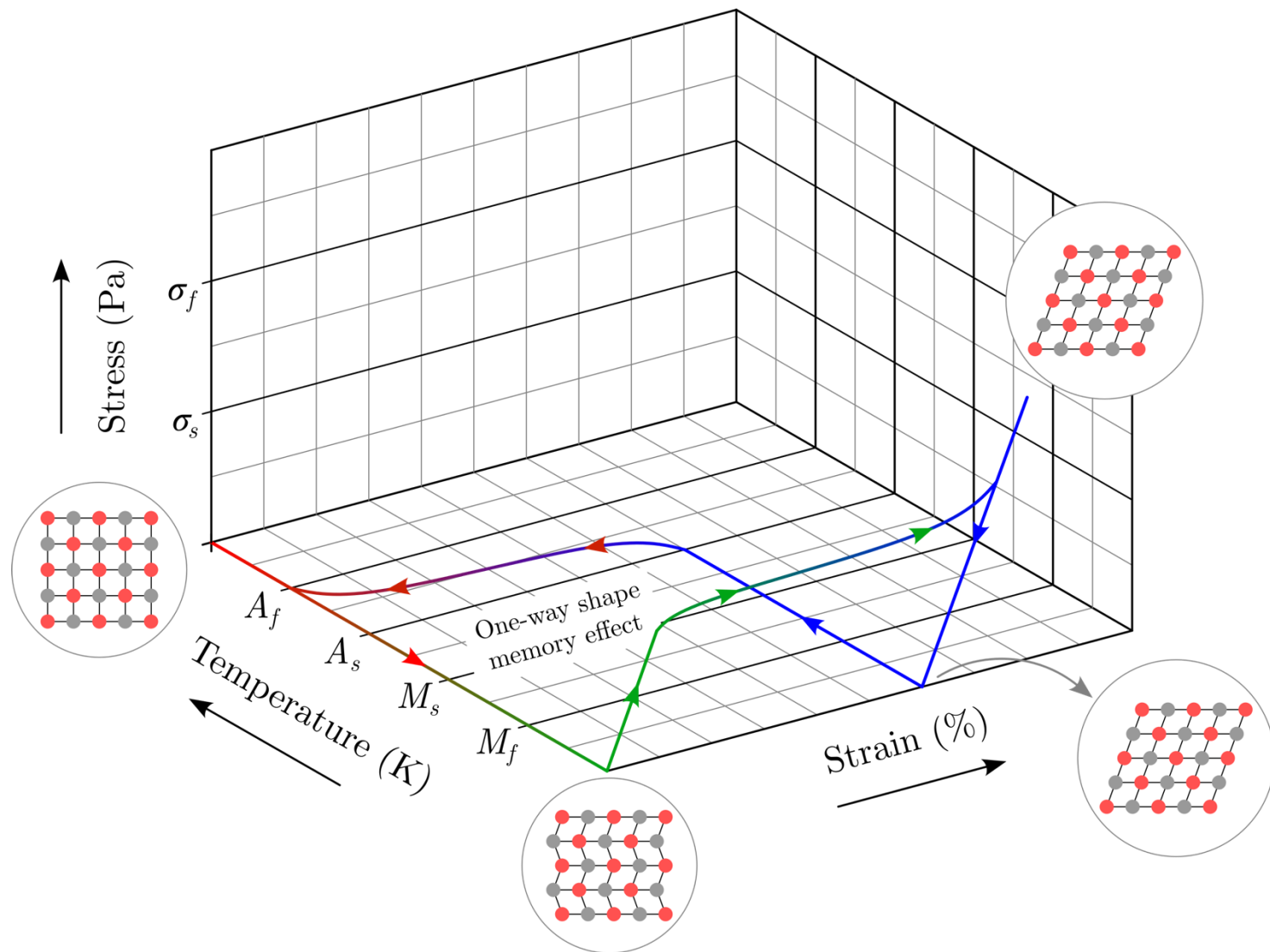


Dornelas (2020)

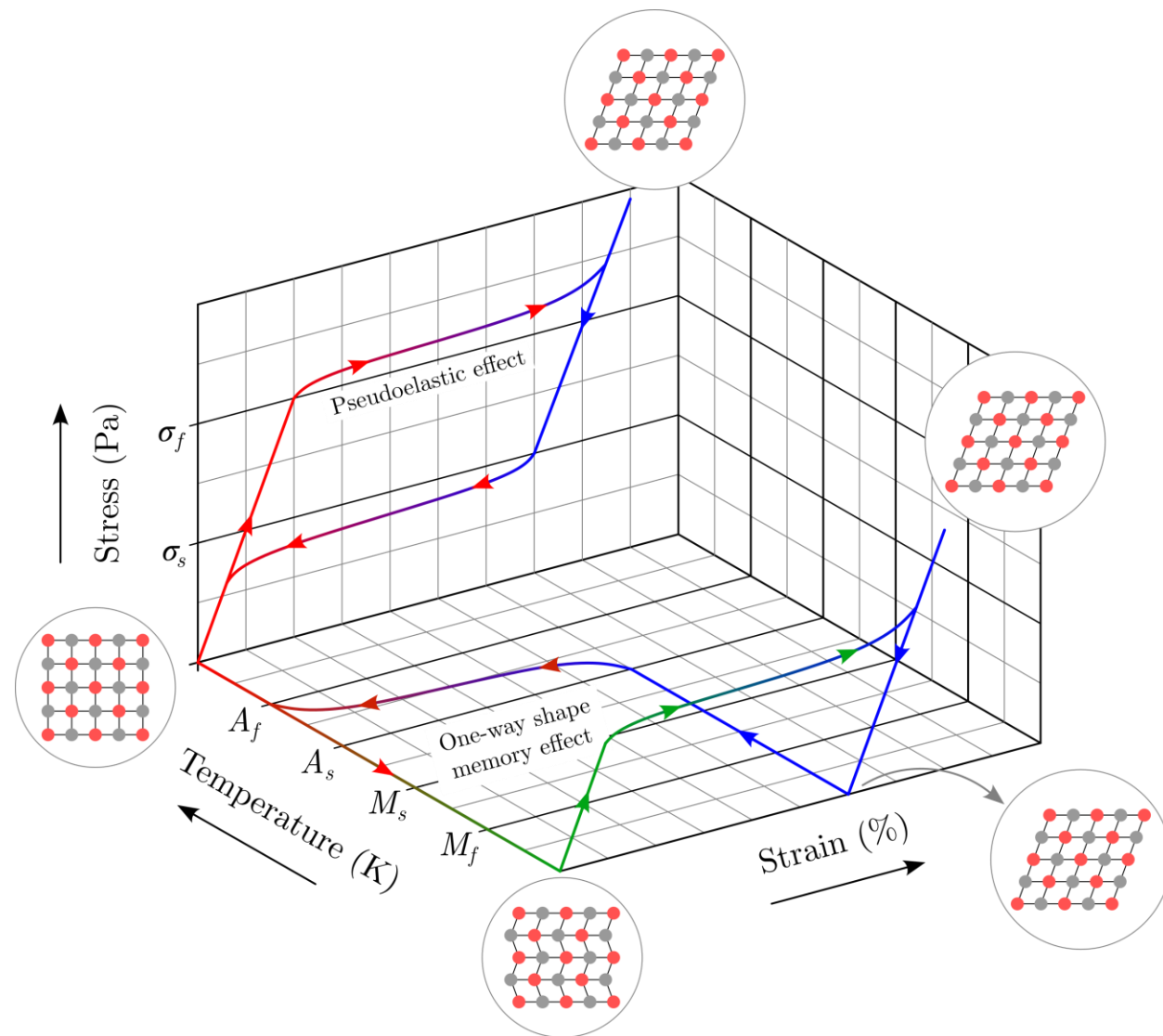
Efeitos Termomecânicos em Ligas SMA

- Efeito Memória de Forma (One-Way)
- Efeito Pseudoelástico
- Transformação de Fase Induzida por Temperatura
- Efeito Memória de Forma Bidirecional (Two-Way)
- Assimetria Tensão-Compressão
- Plasticidade Induzida por Transformação de Fase
- ...

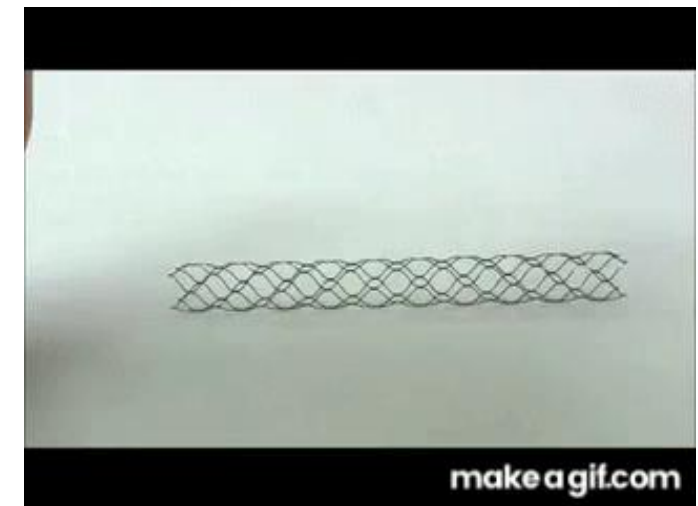
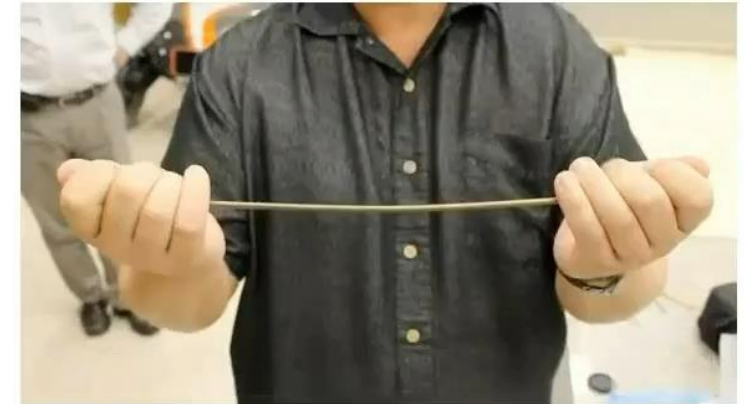
Efeito Memória de Forma



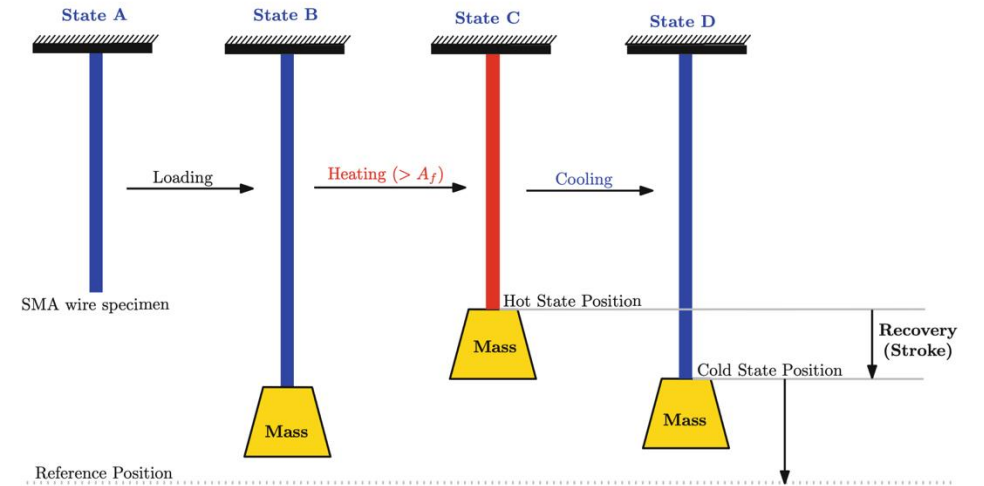
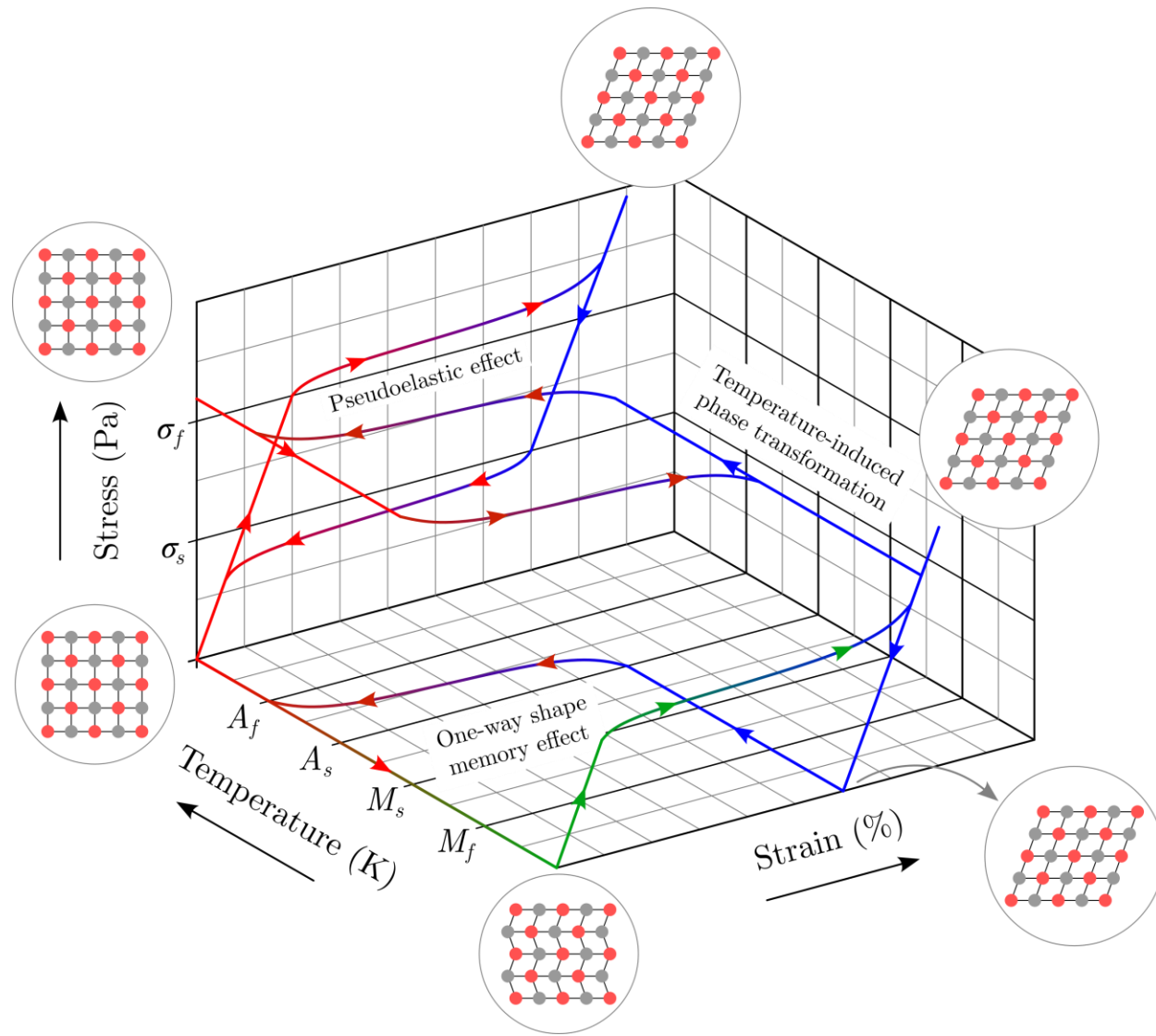
Efeito Pseudoelástico (Superelástico)



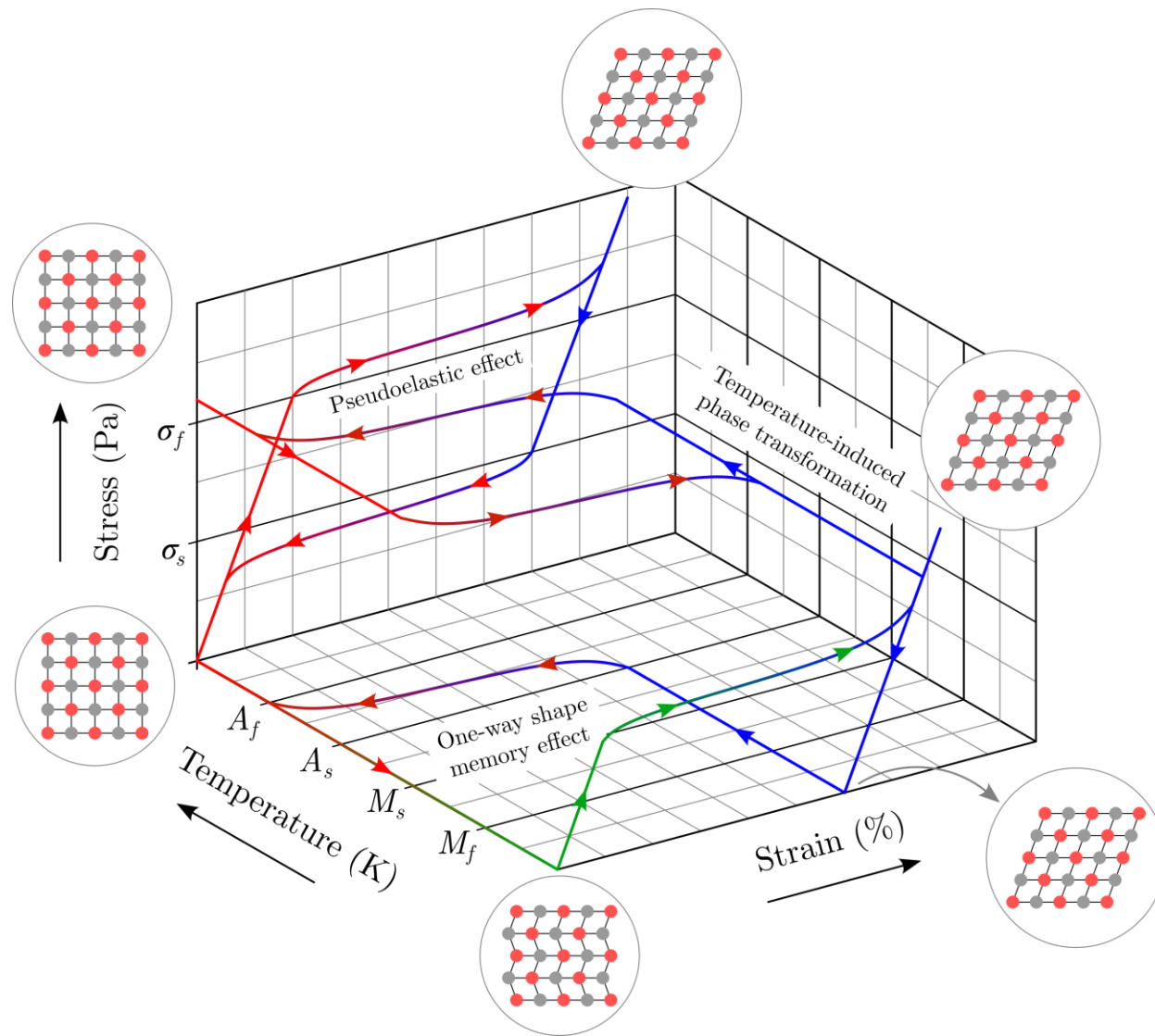
Shape Memory Alloy *Reversible Pseudoelasticity*



Transformação de Fase Induzida por Temperatura



Transformação de Fase Induzida por Temperatura



→ Two-Way Shape Memory Effect
(Bidirecional) se tensão for residual

→ Feita por treinamento (repetição de estímulos específicos diversas vezes)

Equações Constitutivas

$$\boldsymbol{\sigma} = \boldsymbol{\sigma}^R + \boldsymbol{\sigma}^I = \rho \frac{\partial \psi}{\partial \boldsymbol{\varepsilon}} + \frac{\partial \Phi}{\partial \dot{\boldsymbol{\varepsilon}}}$$

$$s = s^R + s^I = - \left(\frac{\partial \psi}{\partial \theta} + \frac{\partial \Phi}{\partial \dot{\theta}} \right)$$

$$\mathbf{B} = -\rho \frac{\partial \psi}{\partial \boldsymbol{\beta}} = \frac{\partial \Phi}{\partial \dot{\boldsymbol{\beta}}}$$

$$\mathbf{g} = -\frac{\partial \Phi}{\partial \mathbf{q}}$$

Modelo Fenomenológico Polinomial de Falk (1980)

$$\boldsymbol{\sigma} = \boldsymbol{\sigma}^R + \boldsymbol{\sigma}^I = \rho \frac{\partial \psi}{\partial \boldsymbol{\varepsilon}} + \frac{\partial \Phi}{\partial \dot{\boldsymbol{\varepsilon}}}$$

$$s = s^R + s^I = - \left(\frac{\partial \psi}{\partial \theta} + \frac{\partial \Phi}{\partial \dot{\theta}} \right)$$

$$B = -\rho \frac{\partial \psi}{\partial \beta} = \frac{\partial \Phi}{\partial \dot{\beta}}$$

$$g = -\frac{\partial \Phi}{\partial q}$$

→ Modelo mais simples de todos

→ Energia livre dependente da deformação cisalhante e temperatura. (Aplicável somente em monocristais).

$$\rho \psi(\varepsilon, \theta) = \frac{a}{2} (\theta - \theta_M) \varepsilon^2 - \frac{b}{4} \varepsilon^4 + \frac{b^2}{24a(\theta_A - \theta_M)} \varepsilon^6$$

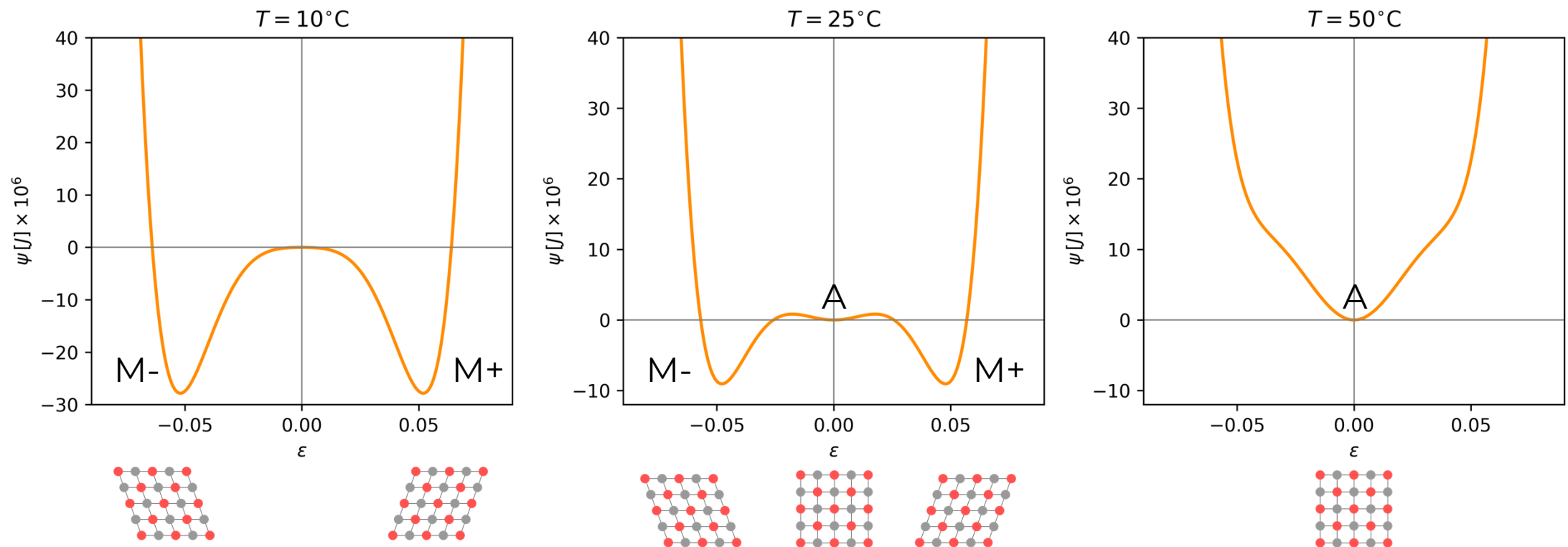
→ Considera fase Austenínica (A), Martensíticas (M+) e (M-)

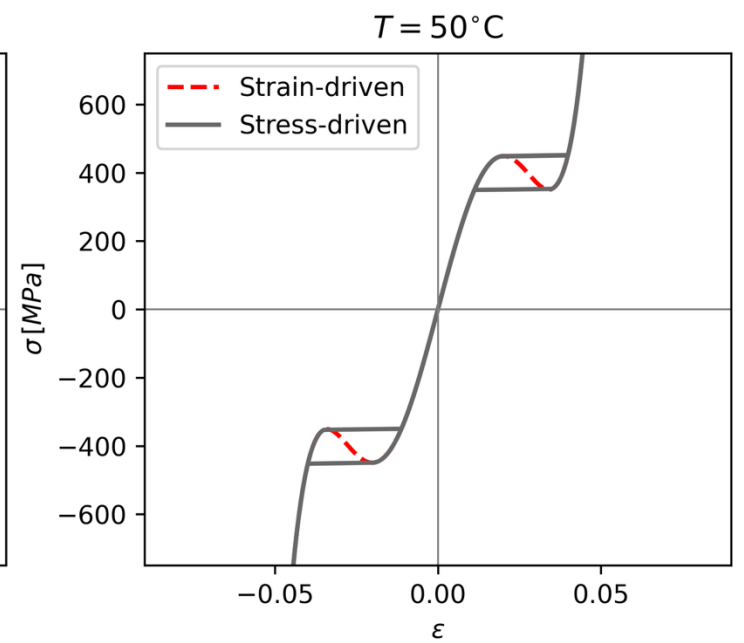
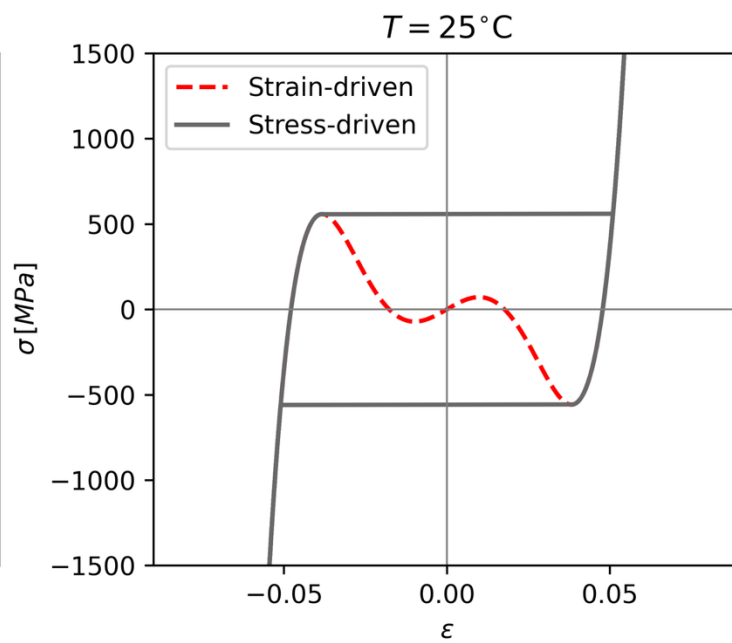
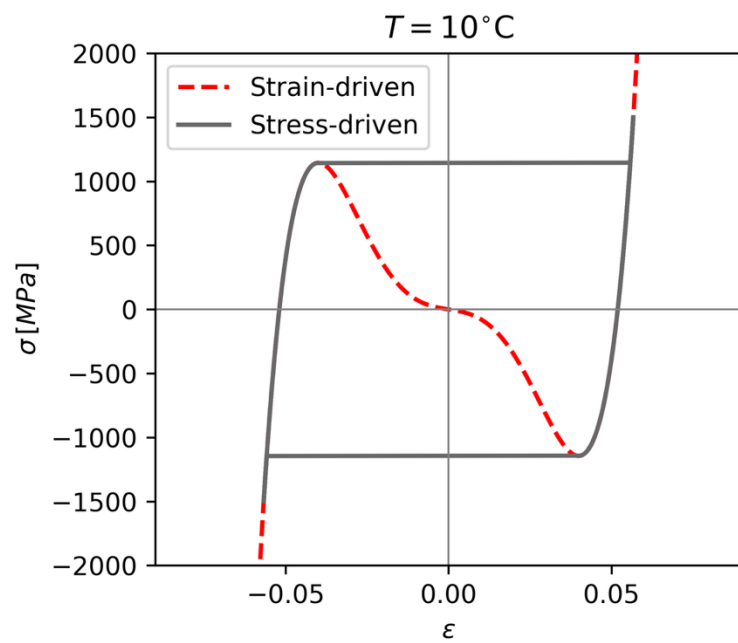
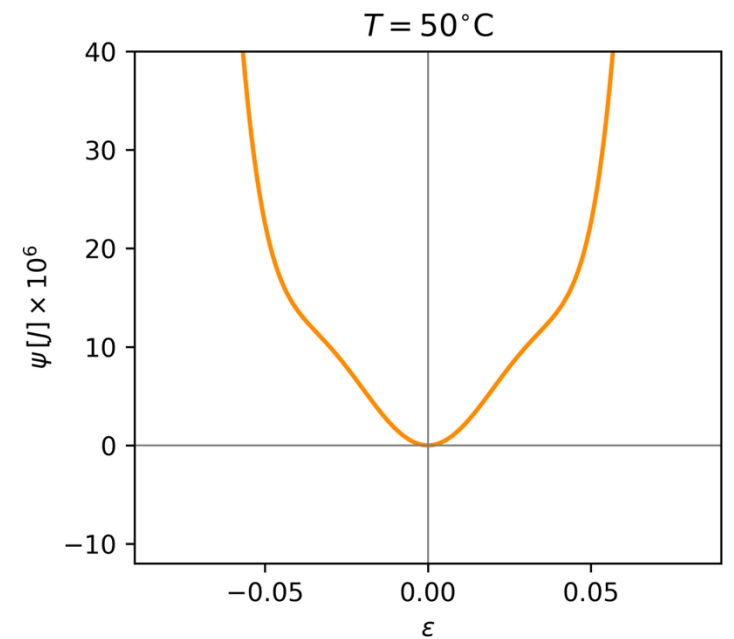
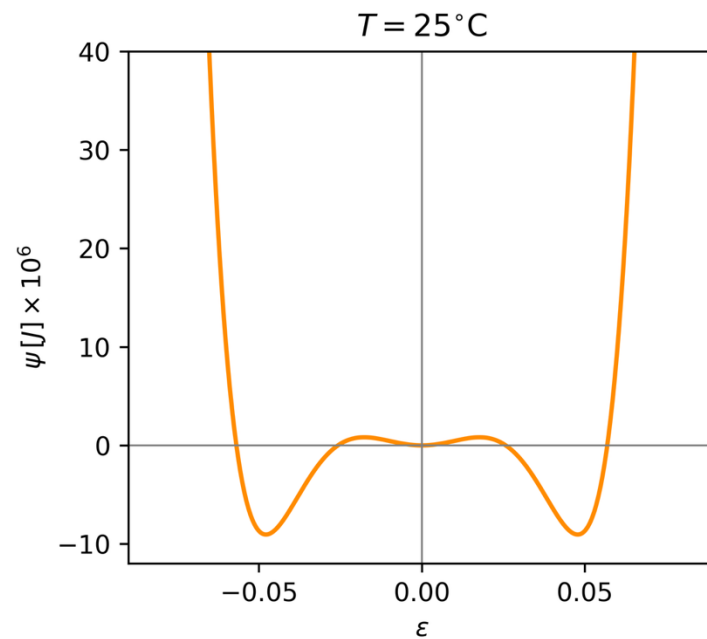
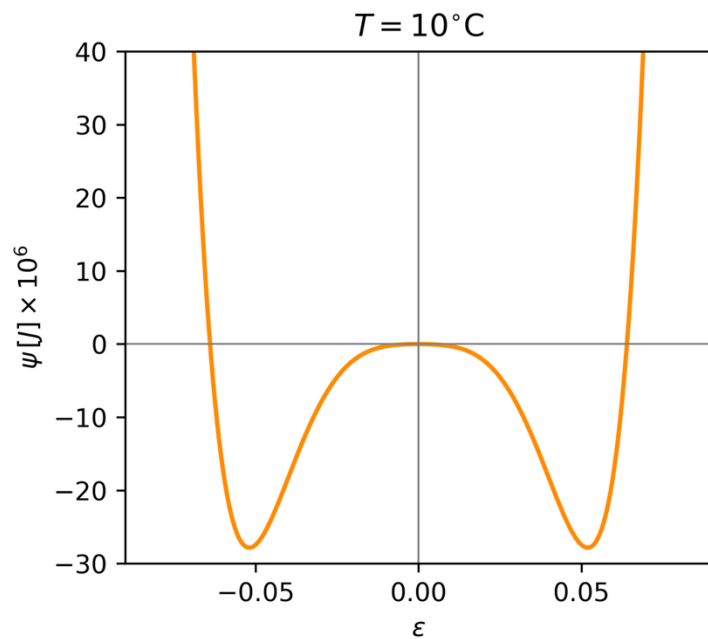
$$\sigma = \rho \frac{\partial \psi}{\partial \varepsilon} = a(\theta - \theta_M) \varepsilon - b \varepsilon^3 + \frac{b^2}{4a(\theta_A - \theta_M)} \varepsilon^5$$

$$s = -\frac{\partial \psi}{\partial \theta} = -\frac{a}{2} \varepsilon$$

Modelo Fenomenológico Polinomial de Falk (1980)

$$\rho\psi(\varepsilon, \theta) = \frac{a}{2}(\theta - \theta_M)\varepsilon^2 - \frac{b}{4}\varepsilon^4 + \frac{b^2}{24a(\theta_A - \theta_M)}\varepsilon^6$$





Modelo de Cinética de Transformação Assumida de Brinson (1993)

→ Considera uma abordagem ligeiramente diferente:

$$\bar{\sigma}(\bar{\varepsilon}, \theta, \beta) = \rho_0 \frac{\partial \psi}{\partial \bar{\varepsilon}}$$

→ Assumindo a forma de taxa:

$$\dot{\bar{\sigma}}(\bar{\varepsilon}, \theta, \beta) = \frac{\partial \bar{\sigma}}{\partial \bar{\varepsilon}} \dot{\bar{\varepsilon}} + \frac{\partial \bar{\sigma}}{\partial \theta} \dot{\theta} + \frac{\partial \bar{\sigma}}{\partial \beta} \dot{\beta}$$

Quantidade de
Martensita no material
($0 \leq \beta \leq 1$)

$$\dot{\bar{\sigma}}(\bar{\varepsilon}, \theta, \beta) = \mathbb{C} \dot{\bar{\varepsilon}} + \gamma \dot{\beta} + \Theta \dot{\theta}$$

Módulo
de
Elasticidade

Tensor
Termoelástico

Tensor Transformação (Mudança de volume durante
Transformação de fase)

Modelo de Cinética de Transformação Assumida de Brinson (1993)

→ A equação constitutiva:

$$\dot{\bar{\sigma}}(\bar{\varepsilon}, \theta, \beta) = \mathbb{C}\dot{\bar{\varepsilon}} + \gamma\dot{\beta} + \Theta\dot{\theta}$$

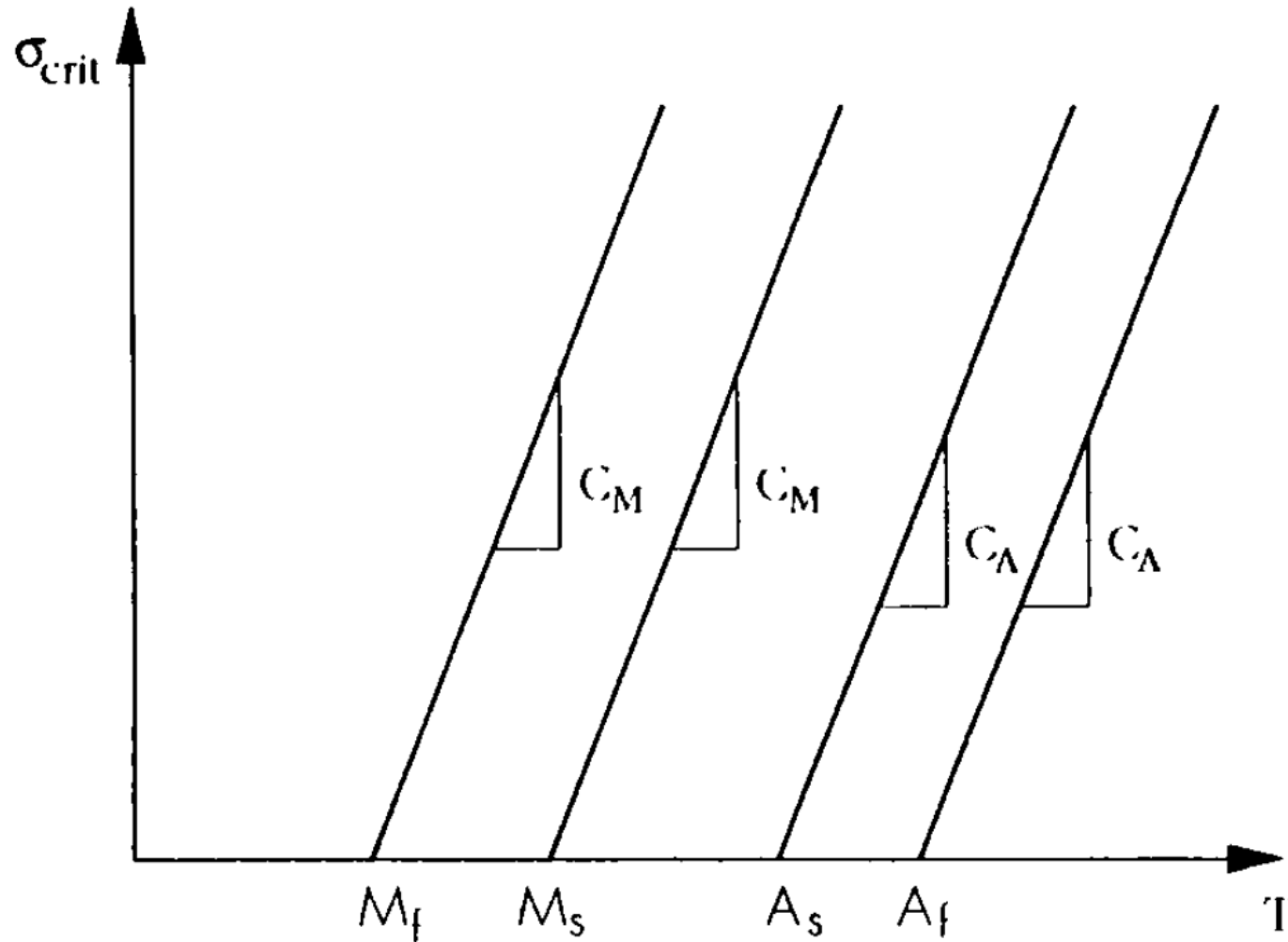
→ Assumindo \mathbb{C} , γ e Θ constantes e integrando no tempo:

$$\int_{t_0}^t \dot{\bar{\sigma}} dt = \int_{t_0}^t [\mathbb{C}\dot{\bar{\varepsilon}} + \gamma\dot{\beta} + \Theta\dot{\theta}] dt$$

$$\bar{\sigma}(t) - \bar{\sigma}(t_0) = \mathbb{C}[\bar{\varepsilon}(t) - \bar{\varepsilon}(t_0)] + \gamma[\beta(t) - \beta(t_0)] + \Theta[\theta(t) - \theta(t_0)]$$

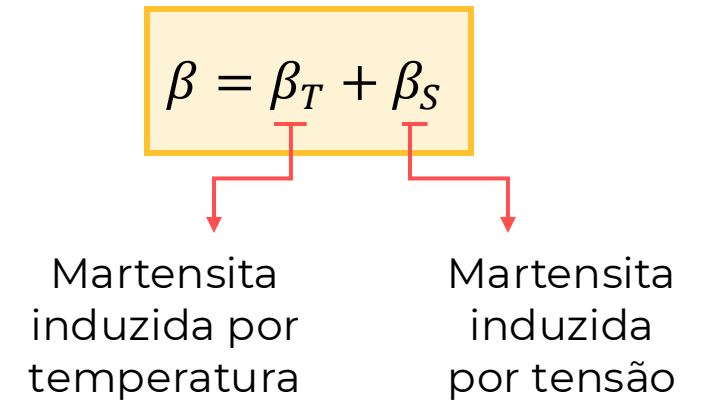
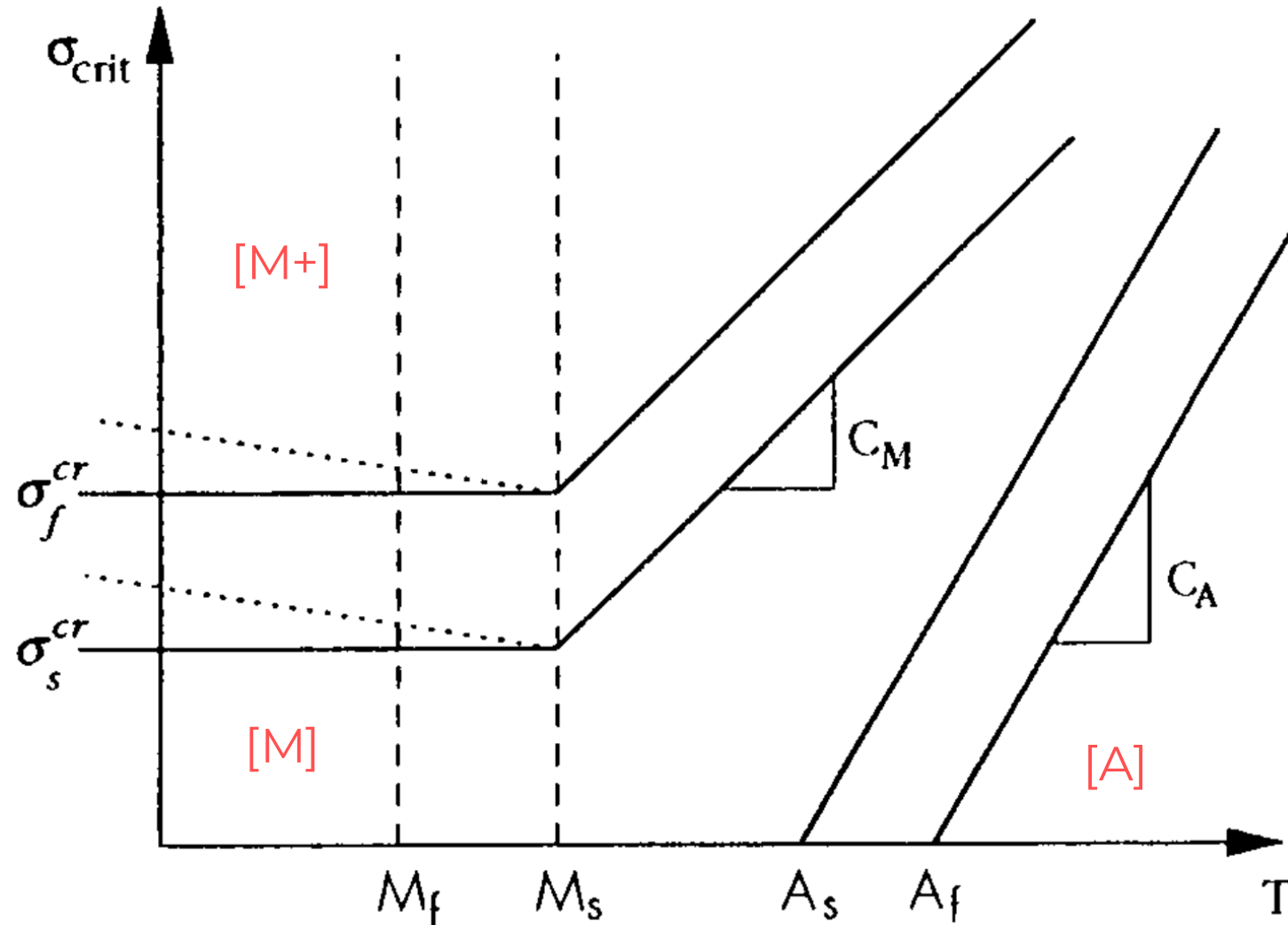
$$\bar{\sigma} - \bar{\sigma}_0 = \mathbb{C}(\bar{\varepsilon} - \bar{\varepsilon}_0) + \gamma(\beta - \beta_0) + \Theta(\theta - \theta_0)$$

Modelo de Cinética de Transformação Assumida de Brinson (1993)



Liang (1990)

Modelo de Cinética de Transformação Assumida de Brinson (1993)



Modelo de Cinética de Transformação Assumida de Brinson (1993)

→ Acoplando a nova condição à equação constitutiva:

$$\bar{\sigma} - \bar{\sigma}_0 = \mathbb{C}(\bar{\varepsilon} - \bar{\varepsilon}_0) + \gamma(\beta - \beta_0) + \Theta(\theta - \theta_0)$$

$$\beta = \beta_T + \beta_S$$

$$\bar{\sigma} - \bar{\sigma}_0 = \mathbb{C}(\bar{\varepsilon} - \bar{\varepsilon}_0) + \gamma_S(\beta_S - \beta_{S0}) + \gamma_T(\beta_T - \beta_{T0}) + \Theta(\theta - \theta_0)$$

Modelo de Cinética de Transformação Assumida de Brinson (1993)

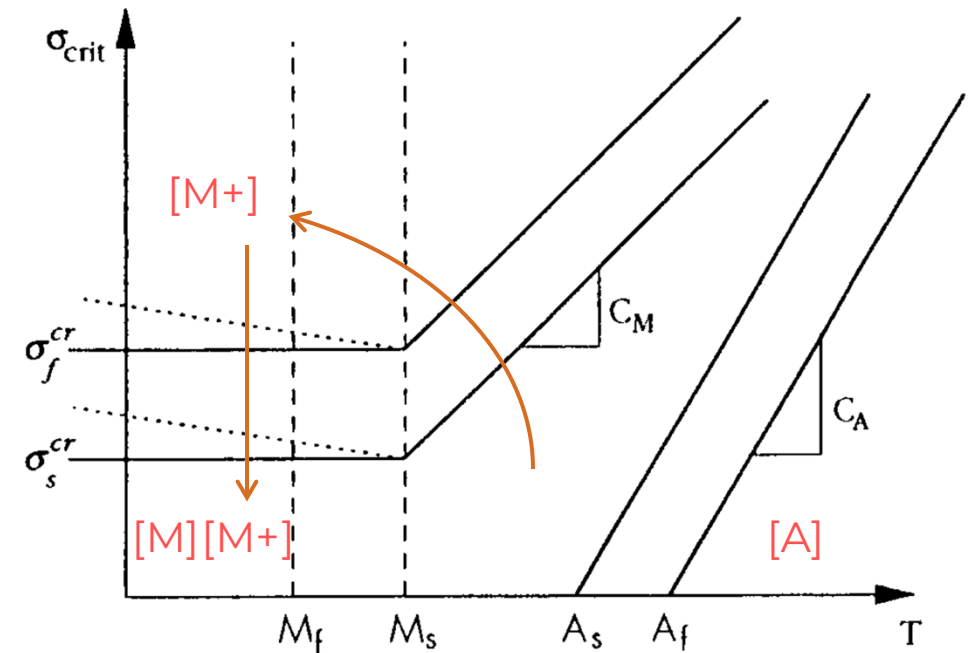
→ A equação constitutiva:

$$\bar{\sigma} - \bar{\sigma}_0 = \mathbb{C}(\bar{\varepsilon} - \bar{\varepsilon}_0) + \gamma_S(\beta_S - \beta_{S0}) + \gamma_T(\beta_T - \beta_{T0}) + \Theta(\theta - \theta_0)$$

→ Aplicando uma transformação máxima de austenita para martensita demacliada, e descarregando após isso:

$$\begin{array}{ll} \bar{\sigma}_0 = \bar{\varepsilon}_0 = 0 & \bar{\sigma} = 0 \\ \beta_{S0} = \beta_{T0} = 0 & \bar{\varepsilon} = \bar{\varepsilon}_R \\ & \beta_S = 1 \\ & \beta_T = 0 \\ & \theta = \theta_0 \quad (M_s > \theta > A_s) \end{array}$$

$$\gamma_S = -\mathbb{C}\bar{\varepsilon}_R$$



Modelo de Cinética de Transformação Assumida de Brinson (1993)

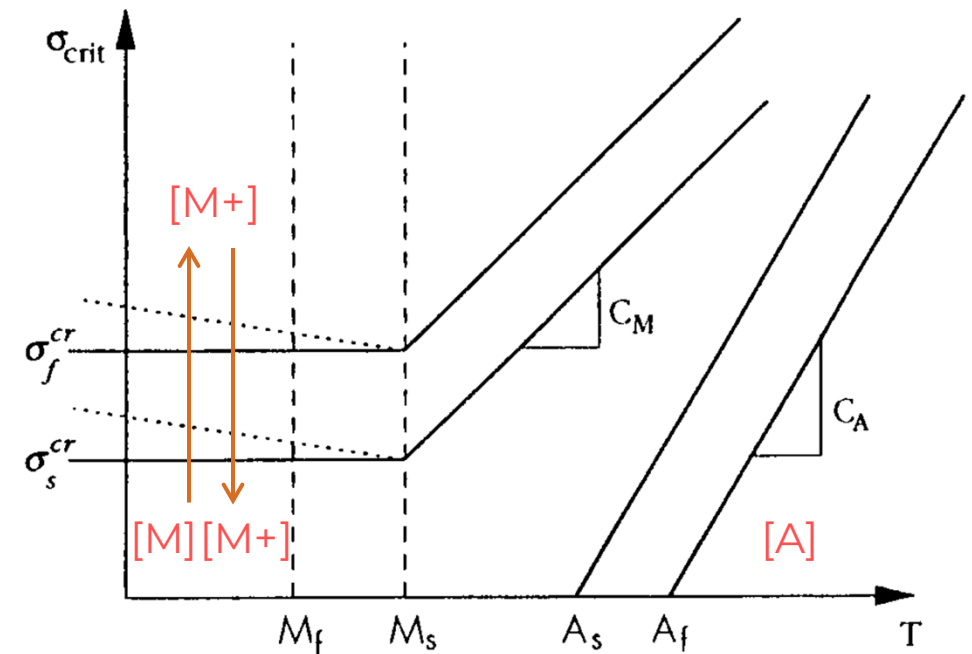
→ A equação constitutiva:

$$\bar{\sigma} - \bar{\sigma}_0 = \mathbb{C}(\bar{\varepsilon} - \bar{\varepsilon}_0) + -\mathbb{C}\bar{\varepsilon}_R(\beta_S - \beta_{S0}) + \gamma_T(\beta_T - \beta_{T0}) + \Theta(\theta - \theta_0)$$

→ Aplicando agora uma transformação máxima de martensita maclada para martensita demaclada, e descarregando após isso :

$$\begin{array}{ll} \bar{\sigma}_0 = \bar{\varepsilon}_0 = 0 & \bar{\sigma} = 0 \\ \beta_{S0} = 0 & \bar{\varepsilon} = \bar{\varepsilon}_R \\ \beta_{T0} = 1 & \beta_S = 1 \\ & \beta_T = 0 \\ & \theta = \theta_0 \end{array}$$

$$0 = \mathbb{C}\bar{\varepsilon}_R - \mathbb{C}\bar{\varepsilon}_R - \gamma_T \longrightarrow \gamma_T = 0$$



Modelo de Cinética de Transformação Assumida de Brinson (1993)

→ A equação constitutiva:

$$\bar{\sigma} - \bar{\sigma}_0 = \mathbb{C}(\bar{\varepsilon} - \bar{\varepsilon}_0) + \gamma_S(\beta_S - \beta_{S0}) + \Theta(\theta - \theta_0)$$

→ Considerando o módulo de elasticidade variável com a fase:

$$\mathbb{C}(\beta) = \mathbb{C}_a + \beta(\mathbb{C}_m - \mathbb{C}_a)$$

Módulo
elástico em
100% de
martensita

Módulo
elástico em
100% de
austenita

→ Resulta em um tensor transformação também variável:

$$\gamma_S(\beta) = -\mathbb{C}(\beta)\bar{\varepsilon}_R$$

Modelo de Cinética de Transformação Assumida de Brinson (1993)

→ Resultando na forma final da equação constitutiva:

$$\bar{\sigma} - \bar{\sigma}_0 = \mathbb{C}(\beta)\bar{\varepsilon} - \mathbb{C}(\beta_0)\bar{\varepsilon}_0 + \gamma_S(\beta)\beta_S - \gamma_S(\beta_0)\beta_{S0} + \Theta(\theta - \theta_0)$$

$$\mathbb{C}(\beta) = \mathbb{C}_a + \beta(\mathbb{C}_m - \mathbb{C}_a)$$

$$\gamma_S(\beta) = -\mathbb{C}(\beta)\bar{\varepsilon}_R$$

→ A evolução de β é assumida ser da forma de cossenos (Transformação assumida)

Conversão para Martensita Demaçada [M+]

Para $\theta > M_s$ e $\sigma_s^{cr} + C_M(\theta - M_s) < \sigma < \sigma_f^{cr} + C_M(\theta - M_s)$:

$$\beta_S = \frac{1 - \beta_{S0}}{2} \cos \left\{ \frac{\pi}{\sigma_s^{cr} - \sigma_f^{cr}} [\sigma - \sigma_f^{cr} - C_M(\theta - M_s)] \right\} + \frac{1 + \beta_{S0}}{2}$$

$$\beta_T = \beta_{T0} - \frac{\beta_{T0}}{1 - \beta_{S0}} (\beta_S - \beta_{S0})$$

Para $\theta < M_s$ e $\sigma_s^{cr} < \sigma < \sigma_f^{cr}$:

$$\beta_S = \frac{1 - \beta_{S0}}{2} \cos \left[\frac{\pi}{\sigma_s^{cr} - \sigma_f^{cr}} (\sigma - \sigma_f^{cr}) \right] + \frac{1 + \beta_{S0}}{2}$$

$$\beta_T = \beta_{T0} - \frac{\beta_{T0}}{1 - \beta_{S0}} (\beta_S - \beta_{S0}) + \Delta_{T\beta}$$

Sendo, se $M_f < \theta < M_s$ e $\theta < \theta_0$:

$$\Delta_{T\beta} = \frac{1 - \beta_{S0}}{2} \left\{ \cos \left[\frac{\pi}{M_s - M_f} (\theta - M_f) \right] + 1 \right\}$$

Caso contrário:

$$\Delta_{T\beta} = 0$$

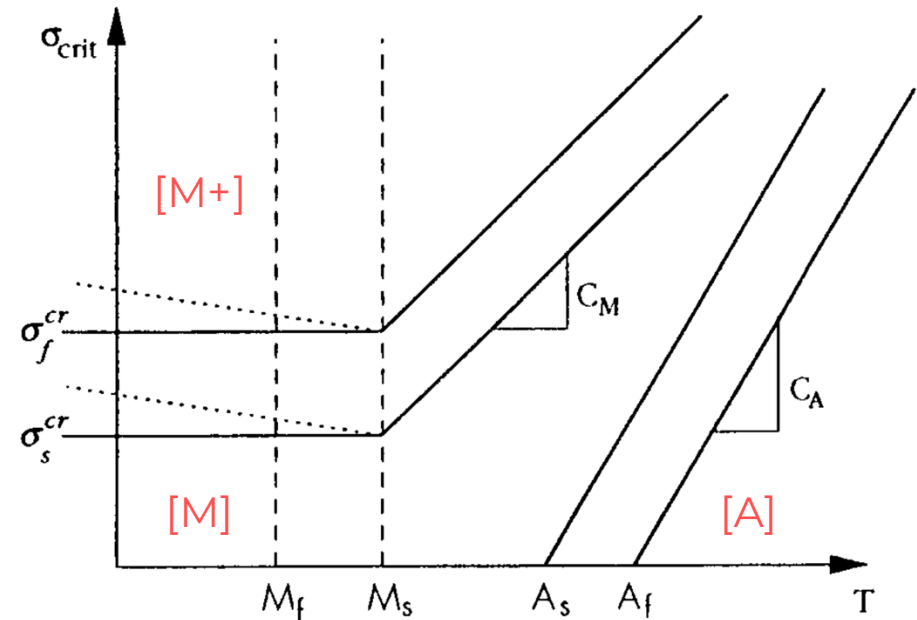
Conversão para Austenita [A]

Para $\theta > A_s$ e $C_A(\theta - A_f) < \sigma < C_A(\theta - A_s)$:

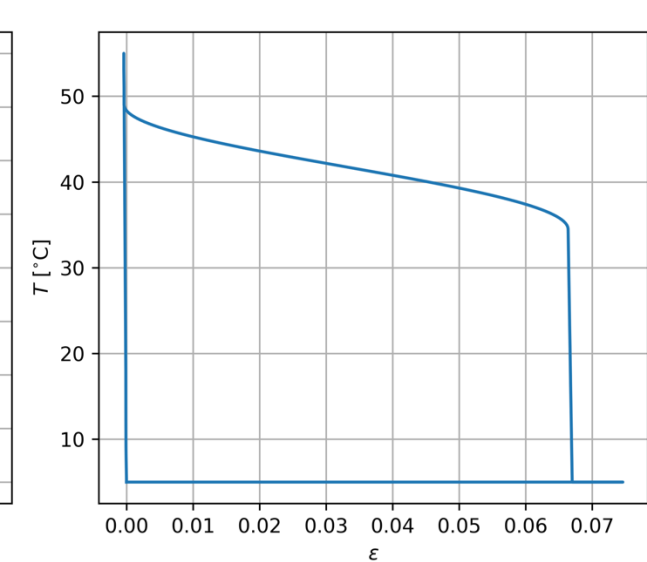
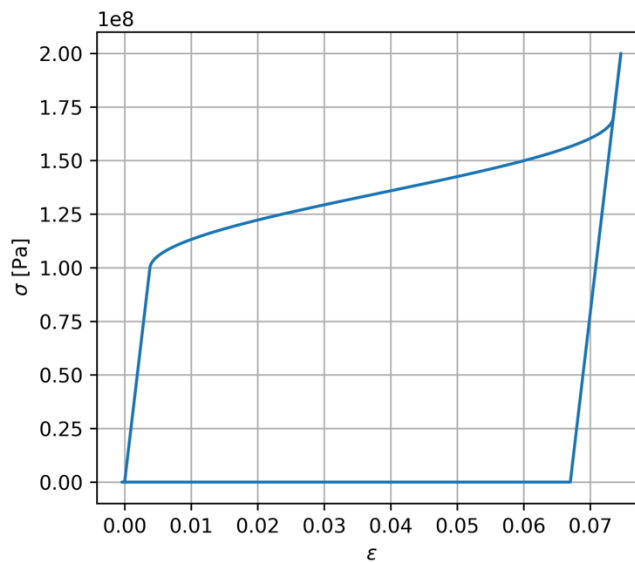
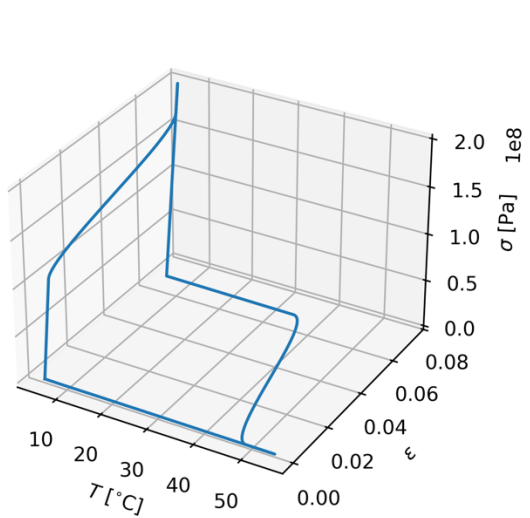
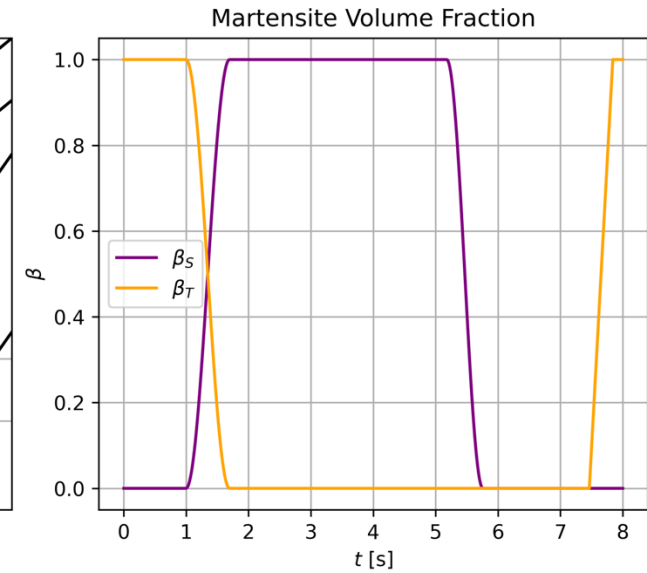
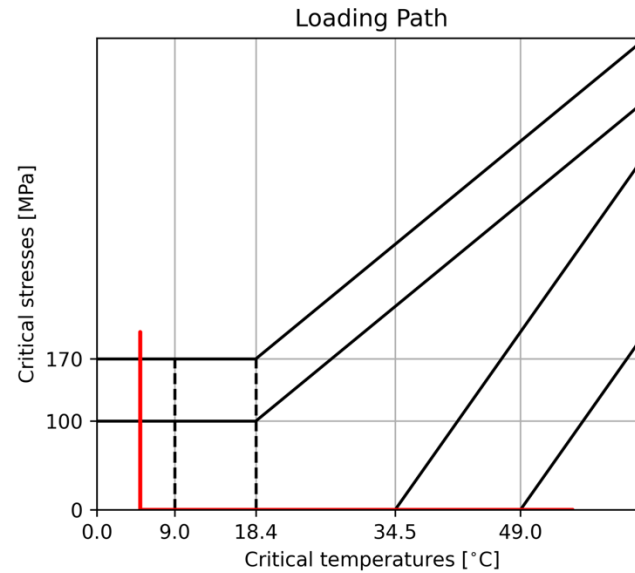
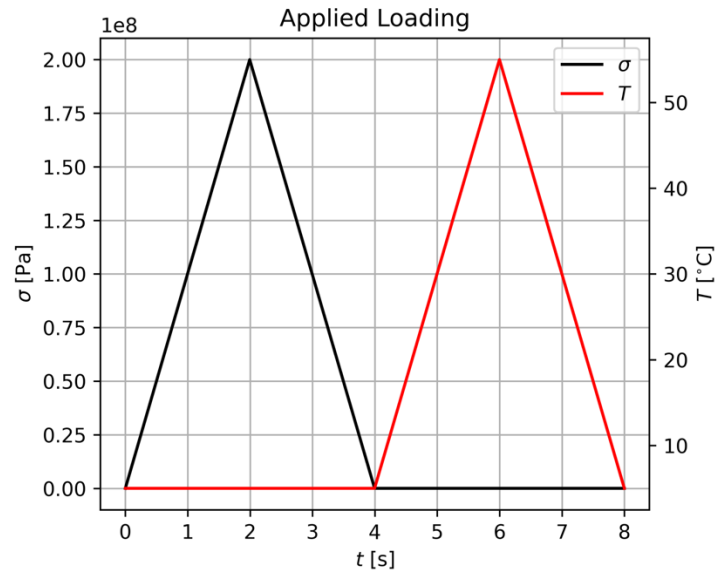
$$\beta = \frac{\beta_0}{2} \left\{ \cos \left[\frac{\pi}{A_f - A_s} \left(\theta - A_s - \frac{\sigma}{C_A} \right) \right] + 1 \right\}$$

$$\beta_S = \beta_{S0} - \frac{\beta_{S0}}{\beta_0} (\beta_0 - \beta)$$

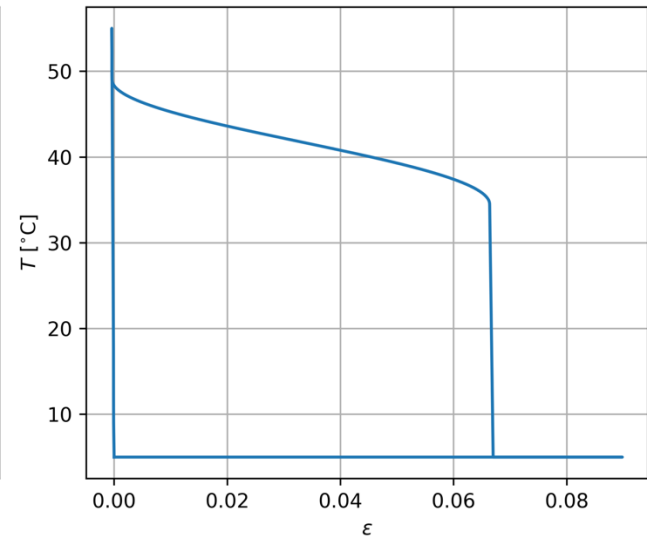
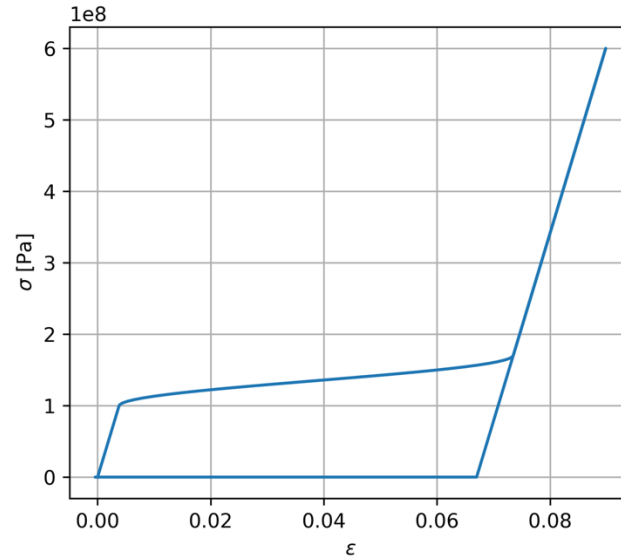
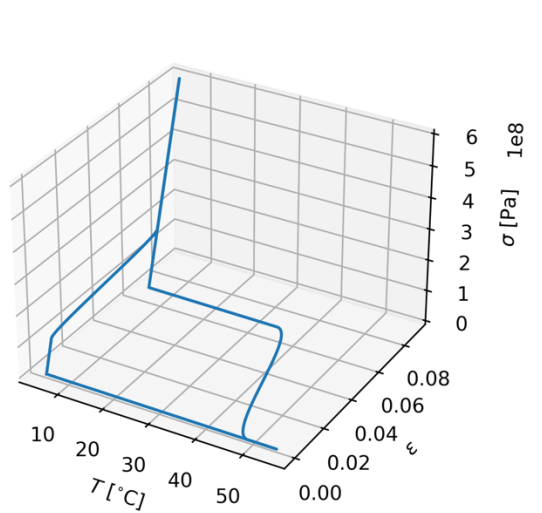
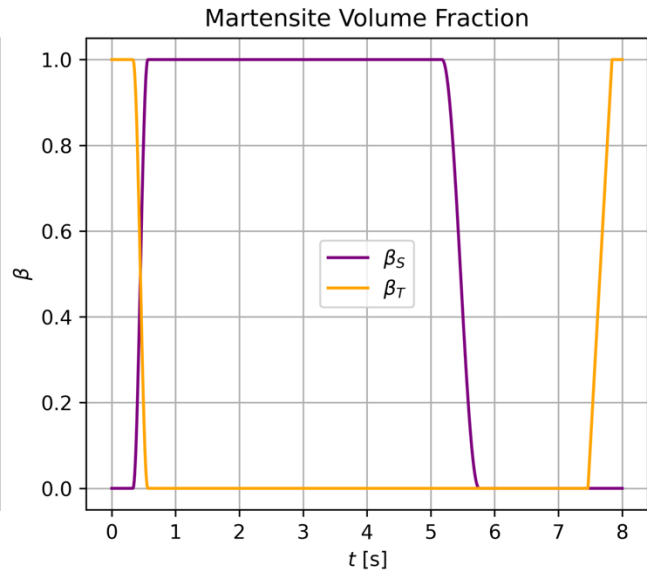
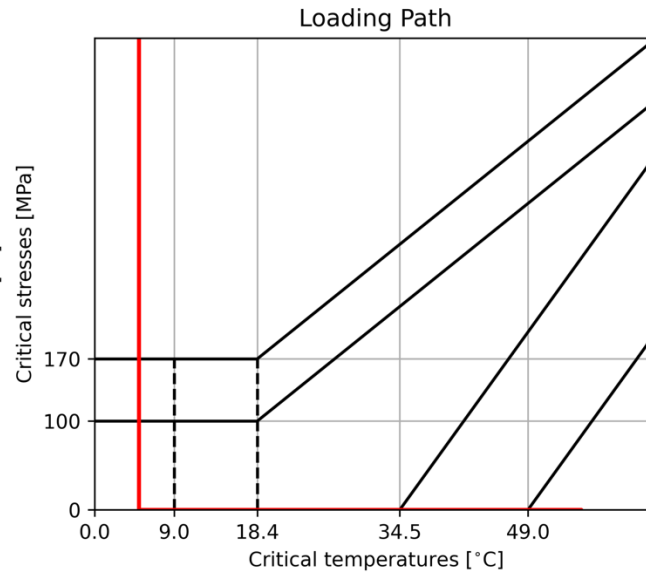
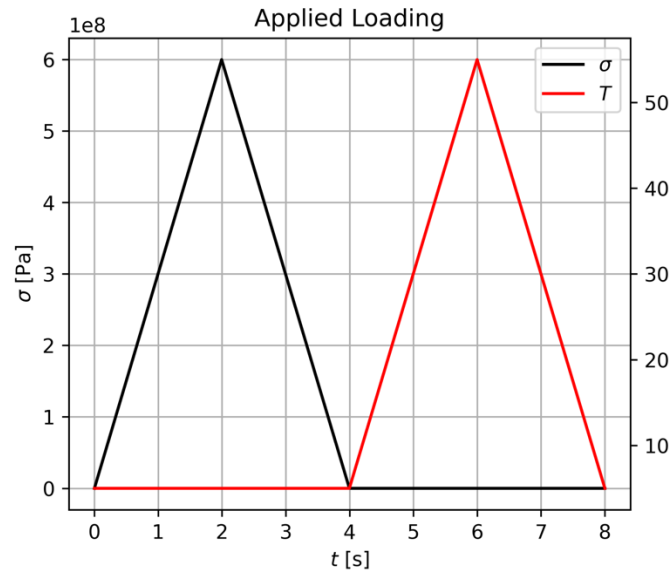
$$\beta_T = \beta_{T0} - \frac{\beta_{T0}}{\beta_0} (\beta_0 - \beta)$$



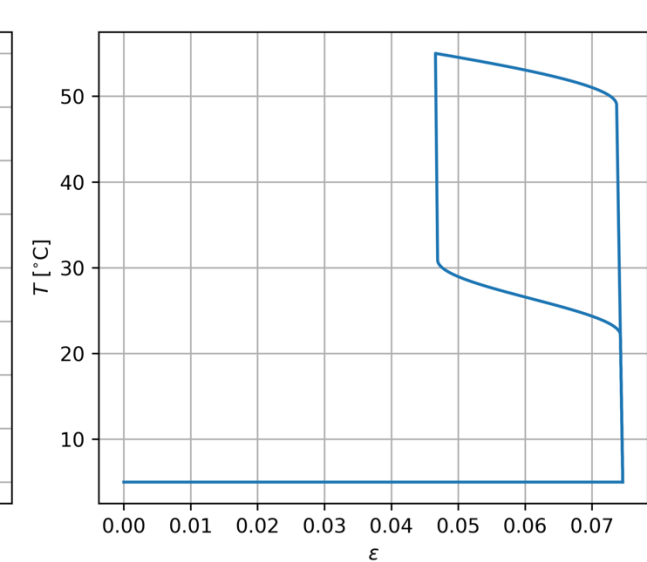
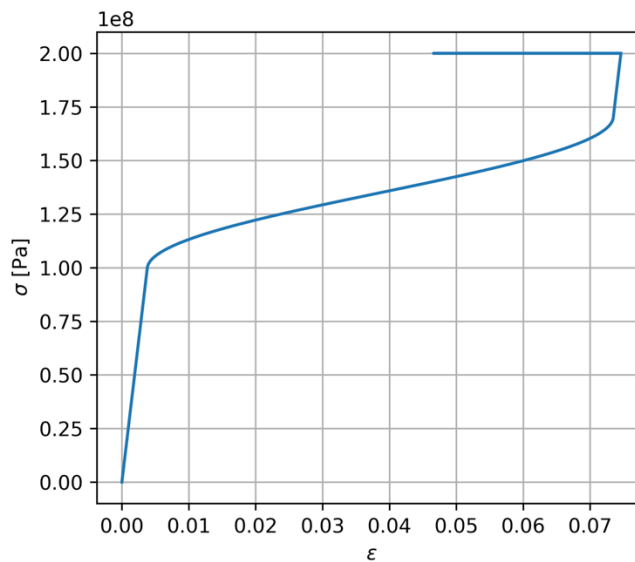
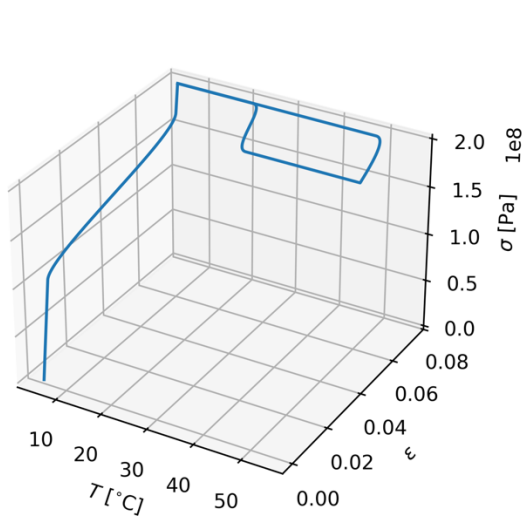
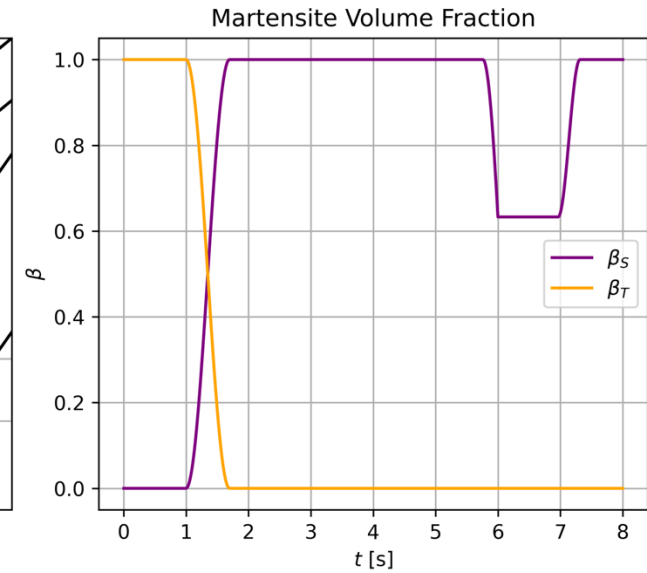
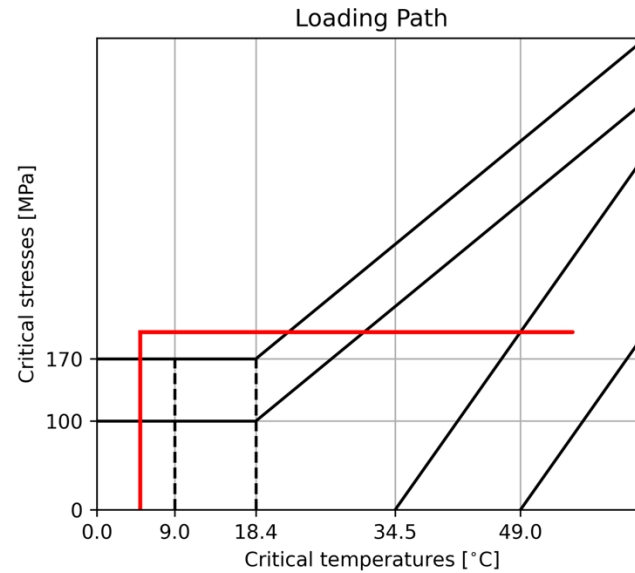
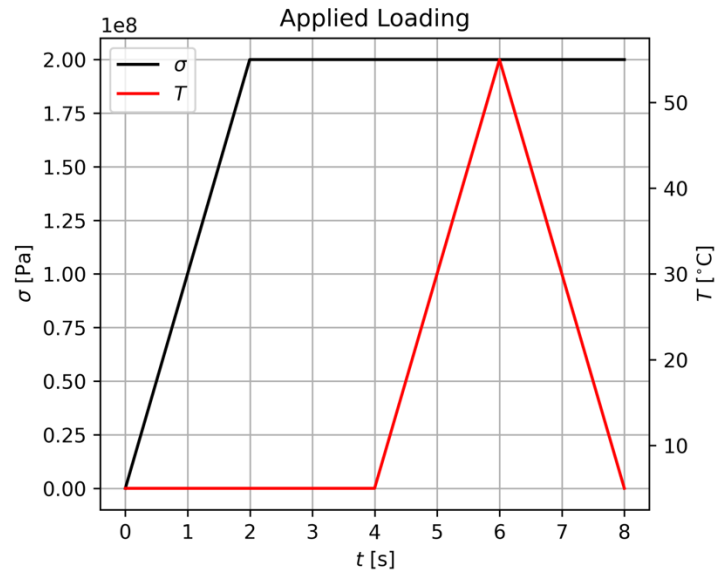
Modelo de Cinética de Transformação Assumida de Brinson (1993)



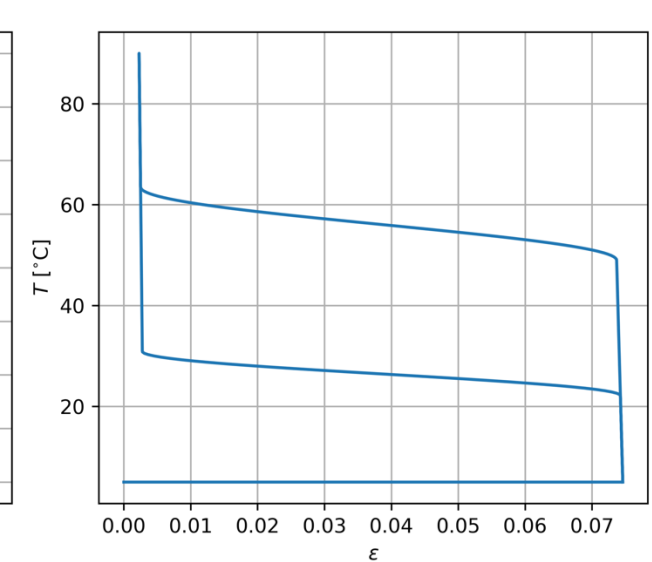
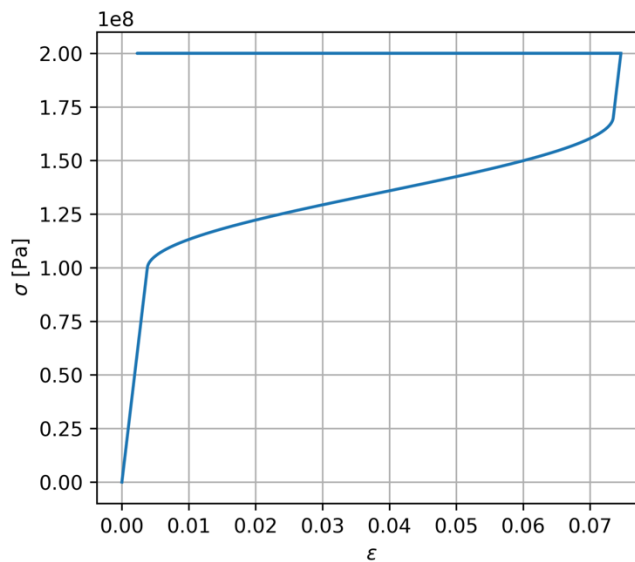
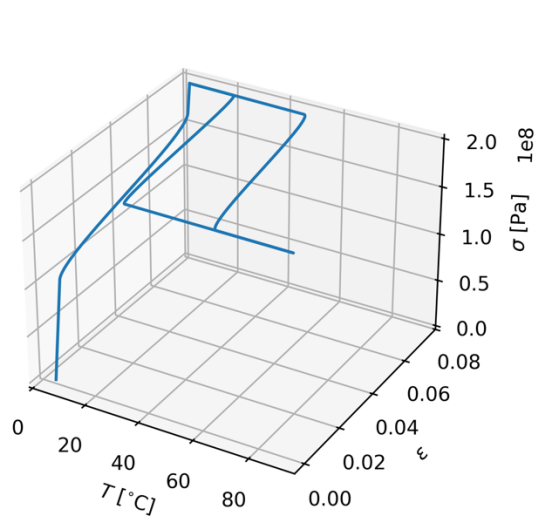
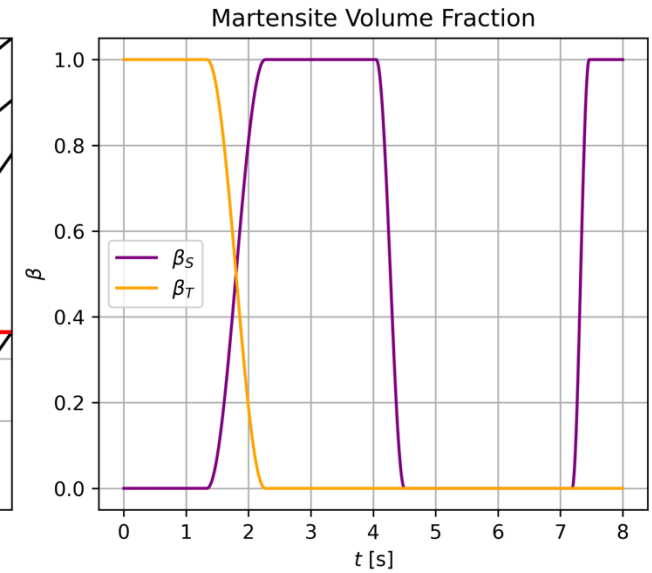
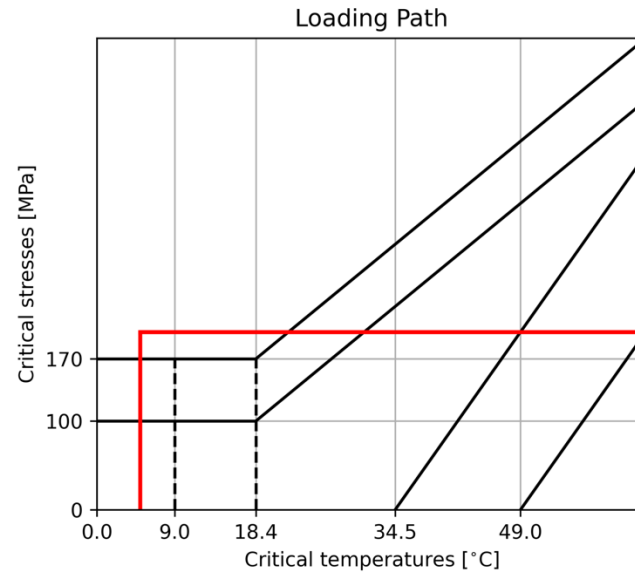
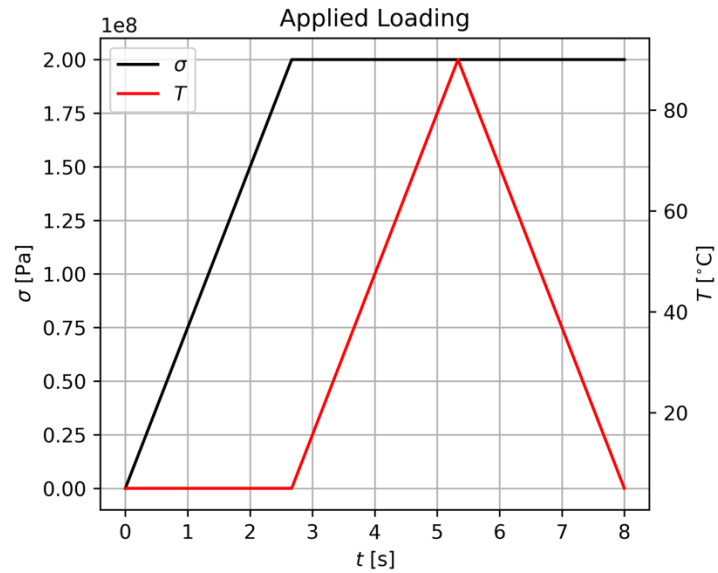
Modelo de Cinética de Transformação Assumida de Brinson (1993)



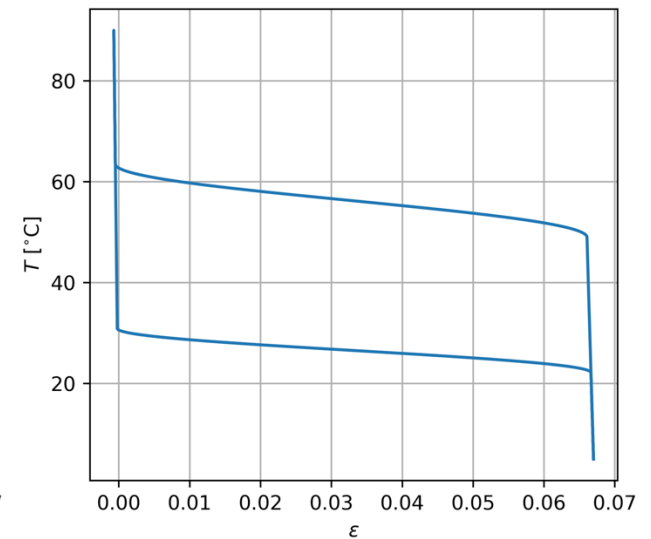
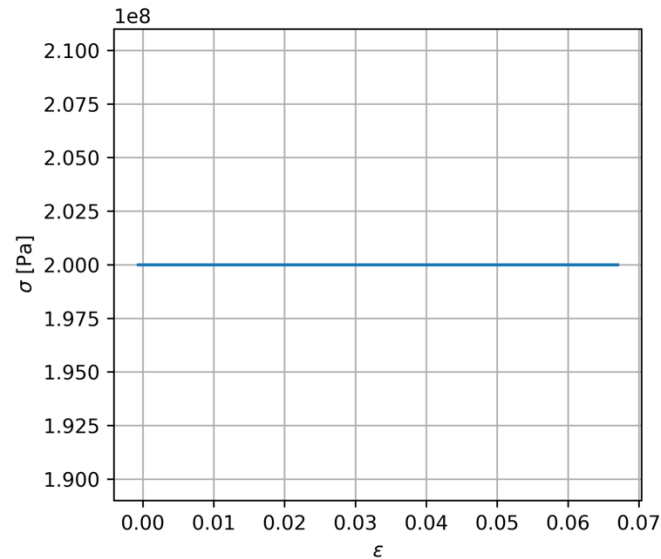
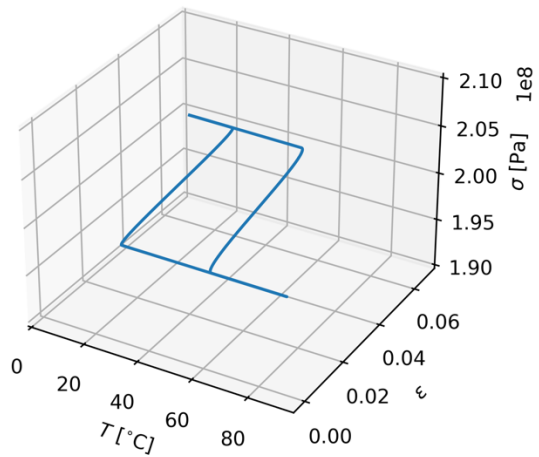
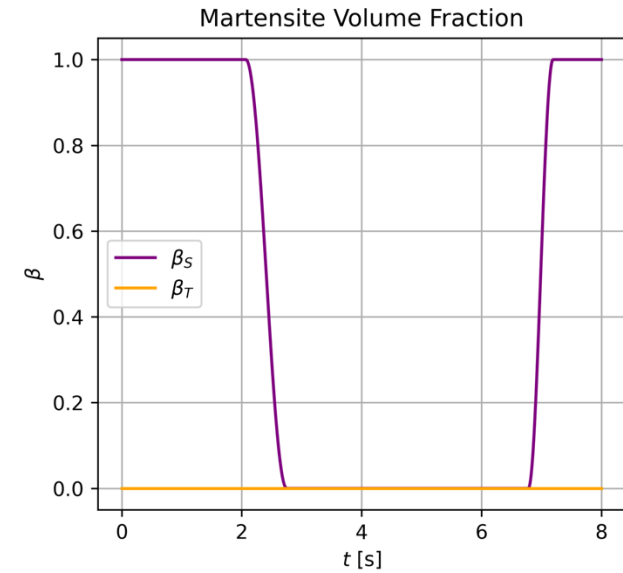
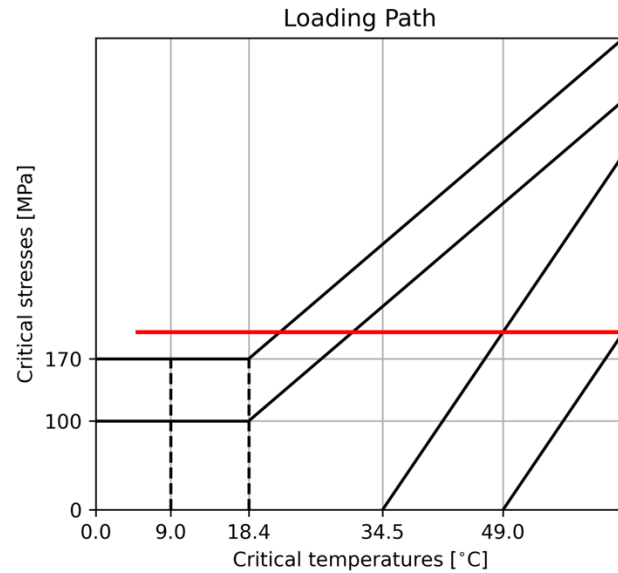
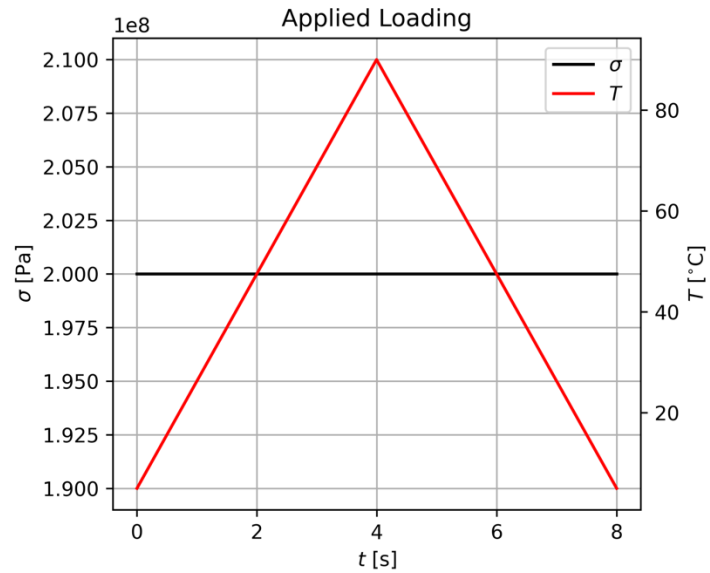
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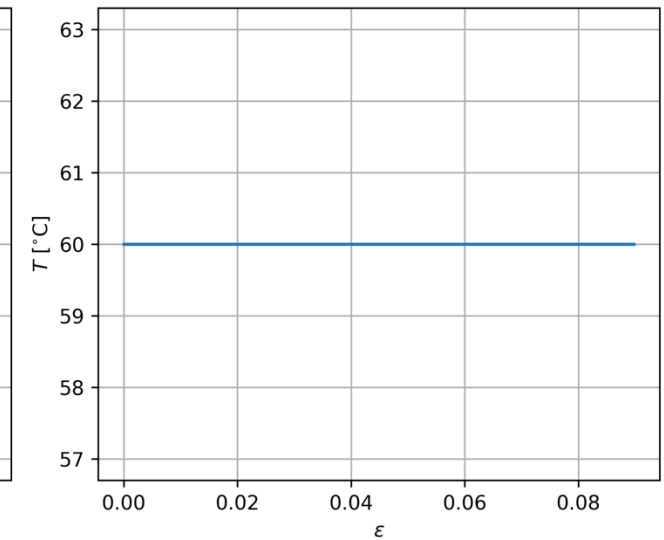
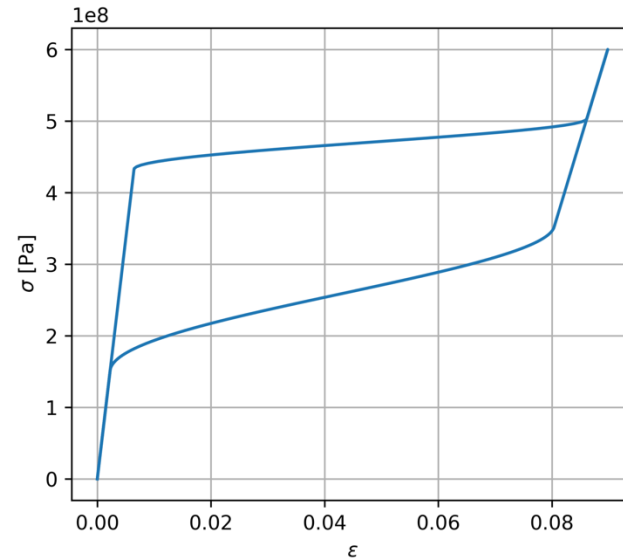
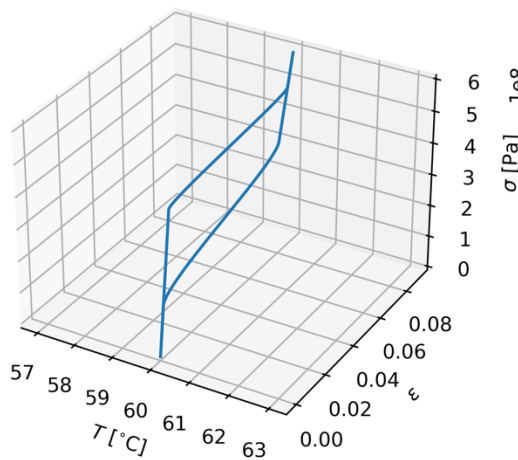
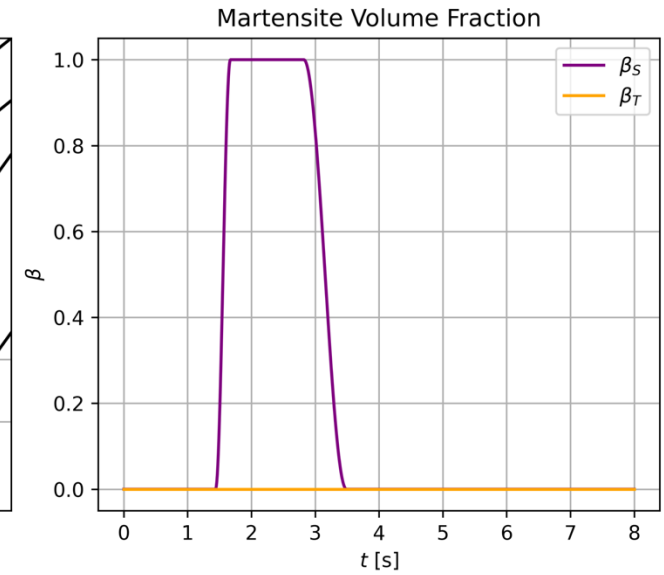
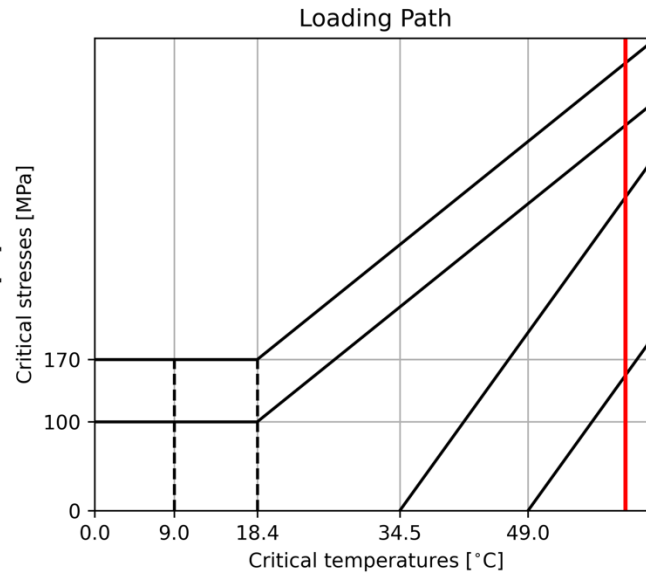
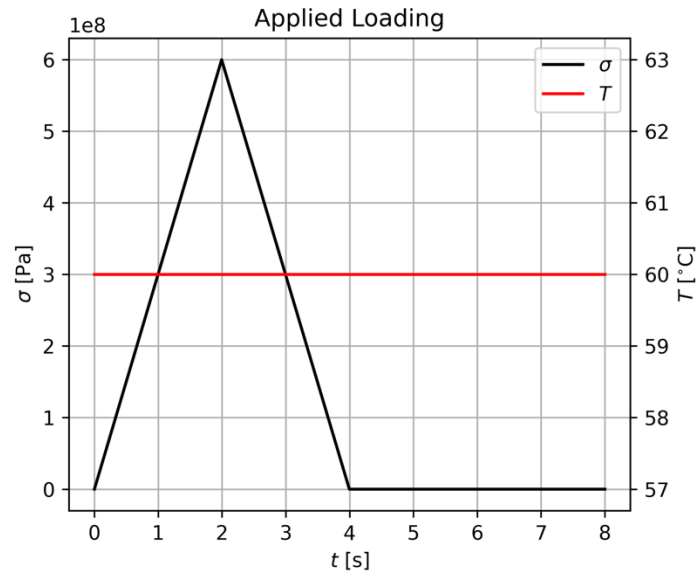
Modelo de Cinética de Transformação Assumida de Brinson (1993)



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